

PRODUCT / PROCESS CHANGE NOTIFICATION PCN-000414 **SEMTECH** Date: Feb 09, 2017

P1/2

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P2/2

List of affected PNs:

Material Composition Declaration:

Pb-free Lens Cap Reliability Qualification Report, (Supplier – Wuhan Risen Tech)

1 Revision History

2 Contents

3 Purpose

The purpose of this report is to document the qualification of Pb-free lens cap for the ROSA products. The lens cap is supplied by Wuhan Risen Tech Co., Ltd.

4 Reliability Qualification Stresses

4.1 Qualification Tests

Table 1.: Qualification Stresses

4.2 Pass Fail Criteria

Temperature Cycling Test Drift Analysis (500 cycles)

M1 and M2 are control parts.

4.3 MS/MV Drift Analysis (1500G, 20-2000Hz)

M1 and M2 are control parts.

4.4 Residual Gas Analysis Results

The RGA content of samples built with Risen cap is acceptable.

5 Conclusion

The Risen lead-free cap is compliant and reliable and can be used in the ROSA products.

GN3250 Characterization Report

(Pb-free lens cap from Risen)

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Revision List

Table of Contents

1. Scope

This document contains a summary of the results of the characterization testing performed on GN3250 ROSA using Pb-free glass seal lens cap from Risen.

2. Method

The GN3250 with LC optical receptacles (barrels) were tested using a Semtech designed evaluation board. These evaluation boards feature controlled impedance lines that are terminated in SMA connectors, and permit full assessment of the electrical properties of the ROSA using input from optical excitation at a wide range of frequencies.

Characterization plan is Gendoc 53406.

3. Results

3.1. Supply Current (I_{CC})

3.1.1. Test Descriptions

In these tests the ROSA was powered up and the current into the V_{cc} pin was measured. During the test the RSSI pin was pulled to ground. The test was performed under the following conditions:

- 1) No optical power input into the ROSA, i.e. P_0 =0mW. This is to test the dark condition.
- 2) 0.5dBm of avg. optical power

The optical signal input to the ROSA was unmodulated. Test was done at both 1310nm and 1550nm.

3.1.2. I_{CC} (no optical input)

3.1.3. I_{CC} (0.5dBm avg. optical power $@$ 1310nm)

3.1.4. I_{CC} (0.5dBm avg. optical power $@$ 1550nm)

3.2. Responsivity, RSSI Dark

3.2.1. Test Descriptions

Responsivity is calculated by dividing the measured the RSSI current by the input optical power at an input optical power of -10dBm (100uW). The input optical signal is unmodulated.

In these tests the ROSA was powered up and the current sunk from the RSSI pin was measured. During the test the RSSI pin was pulled to ground. The test was performed under the following conditions:

- 1) No optical power input into the ROSA, i.e. P_0 =0mW. This is to test the dark condition.
- 2) -10dBm of avg. optical power

The optical signal input to the ROSA was unmodulated. Test was done at both 1310nm and 1550nm.

3.2.4. RSSI dark (nA)

3.3. Optical Receiver Sensitivity

3.3.1. Test Descriptions

The receiver sensitivity tests were performed by performing a sweep of optical powers and recording the BER for those optical powers.

In the case of 10.3125 and 11.3 data rates the output of the ROSA is passed through a GN2013 CDR before reaching the BERT. This is done because the sensitivity of the GN2013 CDR is much better than the BERT inputs and allows for a much better measurement of the true sensitivity of the ROSA.

Figure 1. Sensitivity testing Block Diagram.

Figure 2. 1310nm 11.3Gbps Input Eye Figure 3. 1550nm 11.3Gbps Input Eye

Figure 4. 1310nm 10.3125Gbps Input Eye Figure 5. 1550nm 10.3125Gbps Input Eye

Figure 6. 1310 BaseL Input Eye Figure 7. 1550 BaseL Input Eye

Figure 8. 1310 BaseE Input Eye Figure 9. 1550 BaseE Input Eye

3.3.2. Unstressed Receiver Sensitivity at 1310nm and 11.3Gbps (dBm OMA)

3.3.3. Unstressed Receiver Sensitivity at 1550nm and 11.3Gbps (dBm OMA)

3.3.1. Unstressed Receiver Sensitivity at 1310nm and 10.3125Gbps (dBm OMA)

3.3.2. Unstressed Receiver Sensitivity at 1550nm and 10.3125Gbps (dBm OMA)

3.3.3. Stressed Receiver Sensitivity at 1310nm and BaseL (dBm OMA)

3.3.4. Stressed Receiver Sensitivity at 1550nm and BaseL (dBm OMA)

3.3.5. Stressed Receiver Sensitivity at 1310nm and BaseE (dBm OMA)

3.3.6. Stressed Receiver Sensitivity at 1550nm and BaseE (dBm OMA)

3.4. Optical Overload

3.4.1. Test Descriptions

The optical overload is measured by decreasing the average optical power to the ROSA in steps from a suitable power level.

In the case of 10.3125 and 11.3 data rates the output of the ROSA is passed through a GN2013 CDR before reaching the BERT.

In some cases, the overload test was limited by the maximum optical power of the optical transmitter. As a result, the results in the report only represent a lower bound to the performance of the ROSAs. The ROSA performance is better than results presented in some cases. (Worst case is -40C, 11.3G and 1550nm)

The input eyes used are the same as for the sensitivity tests.

The equipment setup is the same as for the sensitivity tests.

3.4.2. Overload at 1310nm and 11.3Gbps (Avg. power dBm)

3.4.3. Overload at 1550nm and 11.3Gbps (Avg. power dBm)

3.4.4. Overload at 1310nm and 10.3125Gbps (Avg. power dBm)

3.4.5. Overload at 1550nm and 10.3125Gbps (Avg. power dBm)

3.5. Electrical Output Eyes

3.5.1. Test Descriptions

Electrical output eyes of the P channel for the following conditions were measured at 11.3G data rate, unstressed eye at 1550nm wavelength.

1) Average power of -18dBm 2) Average power of -10dBm 3) Average power of 1.6dBm

Eye parameter measurements were made single ended. The following was measured.

1) Crossing Percentage 2) Rise Time 3) Fall Time 4) Eye Height 5) Eye Amplitude 6) Peak to Peak Jitter 7) RMS Jitter

The following tables contain P channel measurements obtained.

The input eyes used are the same as for the sensitivity tests.

The Jitter measurements are uncorrected for jitter of the source.

Long RF cables had to be used to test the ROSAs in a temperature chamber. Due to the attenuation in the RF cables from the ROSA to the scope, the measured parameters of the output eyes are negatively affected. The measured heights and amplitudes are lower than if the signal was directly measured at the output of the ROSA.

For information on the definitions of the eye diagram measurements see Appendix 1

3.5.2. Typical Eye Diagrams at 25C

3.5.1. Typical Eye Diagrams at -40C

3.5.2. Typical Eye Diagrams at 85C

3.5.3. Typical Eye Diagrams at 95C

3.5.4. Crossing Percentage at -18 dBm avg. Power at 1550nm and 11.3Gbps

3.5.5. Rise Time at -18 dBm avg. Power at 1550nm and 11.3Gbps

3.5.6. Fall Time at -18 dBm avg. Power at 1550nm and 11.3Gbps

3.5.7. Height at -18 dBm avg. Power at 1550nm and 11.3Gbps

3.5.10. Jitter RMS at -18 dBm avg. Power at 1550nm and 11.3Gbps

3.5.11. Crossing Percentage at -10 dBm avg. Power at 1550nm and 11.3Gbps

3.5.12. Rise Time at -10 dBm avg. Power at 1550nm and 11.3Gbps

3.5.13. Fall Time at -10 dBm avg. Power at 1550nm and 11.3Gbps

3.5.14. Height at -10 dBm avg. Power at 1550nm and 11.3Gbps

3.5.15. Amplitude at -10 dBm avg. Power at 1550nm and 11.3Gbps

3.5.16. Jitter pk-pk at -10 dBm avg. Power at 1550nm and 11.3Gbps

3.5.17. Jitter RMS at -10 dBm avg. Power at 1550nm and 11.3Gbps

3.5.18. Crossing Percentage at +1.6 dBm avg. Power at 1550nm and 11.3Gbps

3.5.19. Rise Time at +1.6 dBm avg. Power at 1550nm and 11.3Gbps

3.5.20. Fall Time at +1.6 dBm avg. Power at 1550nm and 11.3Gbps

3.5.21. Height at +1.6 dBm avg. Power at 1550nm and 11.3Gbps

3.5.22. Amplitude at +1.6 dBm avg. Power at 1550nm and 11.3Gbps

3.5.23. Jitter pk-pk at +1.6 dBm avg. Power at 1550nm and 11.3Gbps

3.5.24. Jitter RMS at +1.6 dBm avg. Power at 1550nm and 11.3Gbps

3.6. S-parameters

3.6.1. Test Descriptions

An s-parameter sweep was performed with an input optical power of -19dBm and electrical power of 0dBm at 1550nm.

*Note that only 6/10 parts were tested for S-parameters due to equipment availability.

3.6.2. P-Channel S21 plots at 1550nm and -19dBm Optical Input Power

2.97V | 3.3V | 3.63V -400,2.97V,1550 -40C,3.3V,1550 enco any ve -40C 25C, 2.97V, 1550nm 25C.3.3V.1550m 25C.3.63V.1550 25C $\begin{array}{c|c}\n\hline\n & 18 & 2 \\
\hline\n & 18 & 8\n\end{array}$ 14 18 14 18 $\frac{1}{1.8}$ $\frac{1}{\alpha}$ 0.6 85C,2.97V,1550 85C,3.3V,158 85C,3.63V.1 85C $\begin{array}{c|c}\n\hline\n\text{18} & \text{2} \\
\hline\n\text{18} & \text{10}^{\text{y}}\n\end{array}$ $\frac{1}{1}$ 12 $\overline{1.8}$ 95C,3.3V,15 **MC 2.97V** 95C,3.63V.1 95C 7.8 2
 $x = 10^{-7}$ 14 16 $\frac{1}{18}$ 2 $\frac{1}{1.4}$ 16 0.4 0.6 14 16 18

3.6.3. P-Channel S22 plots at 1550nm and 0dBm electrical input power

3.6.4. N-Channel S22 plots at 1550nm and 0dBm electrical input power

3.6.5. S21 -3dB Bandwidth (GHz) at 1550nm

3.6.6. Group Delay (ps) at 1550 nm (6GHz)

4. Notes and Conclusions

GN3250 ROSA using lead free lens cap shows comparable performance to GN3250 ROSA as documented in PRODDOC4073 characterization report.

All results satisfy the datasheet.

5. Appendix 1: Eye Diagram Measurement Definitions

a. Eye Heights

Eye height is a measure of the vertical opening of an eye diagram. Histograms are constructed to characterize both the one and zero levels *and* their noise levels within the eye window boundaries. The one and zero level measurements are made in a section of the eye referred to as the eye window boundaries. The eye window boundary is the central 20% of the bit period.

The one and zero levels are the relative means of the histograms. The noise is measured through the histograms as three standard deviations from both the one level and zero level into the eye opening.

The eye height is determined as follows, eye height = (one level - 3σ) - (zero level + 3σ)

b. Eye Amplitudes

Eye amplitude is the difference between the logic 1 level and the logic 0 level histogram mean values of an eye diagram. This measurement is made in a section of the eye referred to as the eye window boundaries. The eye window boundary is the central 20% of the bit period.

A histogram is constructed using the sampled portion of the eye diagram within the eye window. This histogram is comprised of data points from the upper and lower halves of the eye diagram and is used to determine the mean values of the logic 1 and logic 0 levels. The eye amplitude is determined as follows:

c. Jitter RMS and pk-pk

Eye Jitter is the measure of the time variances of the rising and falling edges of an eye diagram, as these edges affect the crossing point of the eye. To compute jitter, the level of the crossing point of the eye is first determined. Then a vertically thin measurement window is placed horizontally through the crossing point, and a time histogram is generated.

Jitter pk-pk is equal to the full width of the histogram at the eye crossing point.

Jitter RMS is defined as 1 σ (standard deviation) of the crossing point histogram

d. Crossing percentage

Crossing percentage is a measure of the amplitude of the crossing points relative to the one level and zero level. The one and zero level measurements are made in a section of the eye referred to as the eye window boundaries. The eye window boundary is the central 20% of the bit period.

A vertically thin measurement window is placed horizontally through the crossing points, and a horizontal histogram is used to determine the mean location (in time) of the crossing point.

A narrow vertical histogram is used to determine the amplitude of crossing points.

The mean derived from the horizontal and vertical histogram results in V_{cross} . Crossing percentage is then determined by the following:

Crossing percent = 100 (V_{cross} - V_{zero level)/(V_{one} level – V_{zero} level)

e. Rise Time and Fall Time

Rise time is a measure of the mean transition time of the data on the upward slope of an eye diagram. The data crosses through the following three thresholds: the lower, middle, and upper thresholds, as well as through the eye crossing point. The settings for the threshold levels are the 20% to 80% points on the transition.

Rise time= time at the upper threshold crossing – time at the lower threshold crossing Fall times are similarly calculated except on the downward slope of an eye diagram.