

PRODUCT / PROCESS CHANGE NOTIFICATION PCN-000414 Date: Feb 09, 2017

P1/2

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	,,,						
	Change	e Details					
Part Number(s) Affecte	ed: Cu	stomer Part Number(s)	Affected: 🛛 N/A				
Product families GN32xx and	d GN33xx						
Full list attached below.							
Description, Purpose a	and Effect of Change:						
Introducing Pb-free lens ca	ap eliminating RoHS exem	otion no 7(c) from LR ROSA p	products.				
Replacing lens cap from S seal that is Pb-free.	Schott using Pb in glass s	eal with ball lens cap from	Wuhan Risen using glass				
Change Classification	🖂 Major 🗌 Minor	Impact to Form, Fit, Function	🗌 Yes 🛛 No				
Impact to Data Sheet	🗌 Yes 🛛 No	New Revision or Date	⊠ N/A				
Impact to Performance	e, Characteristics or R	eliability:					
- Porformanco Charactorist	ice and Poliability are not a	affected as per attached docu	Imontation				
renormance, characterist	ics and Kenability are not a	anected as per attached docu					
Implementation Date	July 1, 2017	Work Week					
Last Time Ship (LTS)	NA	Affecting Lot No. /	NA				
Of unchanged product	March 40, 2047	Serial No. (SN) Qualification Report	Available				
Sample Availability	March 10, 2017	Availability	Available				
Supporting Document	s for Change Validatio	on/Attachments:					
Characterization Re	eport – PRODDOC013839						
 Reliability Report – 							
 Material Compositi 	on Declaration for Lens Ca	lb in the second s					
		Authority					



PRODUCT / PROCESS CHANGE NOTIFICATION PCN-000414 Date: Feb 09, 2017

P2/2

Semtech Business Unit:	Signal Integrity Group				
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FOR FURTHER INFORMATION & WORLDWIDE SALES COVERAGE: <u>http://www.semtech.com/contact/index.html#support</u>					

List of affected PNs:

GN3250	GN3252	GN3268	GN3257	GN3270	GN3352	GN3357	GN3368	GN3358
GN3250-3EF7AM6E3	GN3252-3EB8AN3E3	GN3268-3EB7AN9E3	GN3257-3EB9AU2E3	GN3270-3EC7AV3E3	GN3352-3EB8AR9E3	GN3357-3EB9AV5E3	GN3368-3EC8AT6E3	GN3358-3EF8AT6E3
GN3250-3EG7AM6E3	GN3252-3EB8AT3E3	GN3268-3EB7AM2E3	GN3257-3EB9AV4E3	GN3270-3EC7AV8E3	GN3352-3EB8AT4E3	GN3357-3EB9AQ9E3	GN3368-3EC8AT8E3	GN3358-3EF8AU2E3
GN3250-3EB7AM2E3		GN3268-3EB7AV4E3	GN3257-3EB9AT5E3	GN3270-3EC7AV9E3	GN3352-3EB8AQ4E3	GN3357-3EB9AS6E3	GN3368-3EC8AU8E3	GN3358-3EF8AT8E3
GN3250-3EB7AK8E3		GN3268-3EB7AS9E3	GN3257-3EB9AP6E3		GN3352-3EB8AQ7E3	GN3357-3EB9AN4E3	GN3368-3EC9AT6E3	GN3358-3EF8AV6E3
GN3250-3EB7AQ5E3		GN3268-3EB7AT2E3			GN3352-3EB8AQ9E3	GN3357-3EB9AT6E3	GN3368-3EC9AT8E3	
GN3250-3EB7AP6E3		GN3268-3EB7AR2E3			GN3352-3EB8AR4E3	GN3357-3EB9AT9E3	GN3368-3EC8AN4E3	
GN3250-3EB7AN9E3		GN3268-3EB7AU2E3			GN3352-3EB8AR6E3	GN3357-3EB9AU2E3	GN3368-3EC8AU6E3	
GN3250-3EB7AP2E3		GN3268-3EB7AP6E3			GN3352-3EB8AS6E3	GN3357-3EB9AU4E3		
GN3250-3EG7AR2E3		GN3268-3EB7AM6E3			GN3352-3EB8AV5E3	GN3357-3EB9AU7E3		
GN3250-3EB7AM6E3		GN3268-3EB7AM7E3						
GN3250-3EB7AM7E3		GN3268-3EB7AM8E3						
GN3250-3EB7AM8E3		GN3268-3EB7AT8E3						
GN3250-3EB7AN4E3		GN3268-3EH8AN3E3						

Material Composition Declaration:

		-				
	Material	Composition				
Product	RX.CBY.12755					
Package	Lens cap Pb-free	(Wuhan Risen Tecl	n Co.)			
Manufacturer	Semtech Corpora				Date	12/15/201
		Weight of		Weight of	Homogeneous m	aterial
Component	Subcomponent	Component	Substance		%	pp
		ma		ma		
Ball LensCap	Base	83.00	с	0.00	0.001	1
			Si	0.13	0.160	160
			Mn	0.66	0.800	800
			P	0.00	0.004	4
			s	0.00	0.002	2
			Ni	41.56	50.070	50070
			Co	0.01	0.010	10
			Cr	0.01	0.010	10
			AI	0.01	0.010	10
			Fe	40.61	48.933	48933
			Subtotal	83.00	100.00	100000
	Solder Glass	6.60	Proprietry	1.80	No Lead	100000
	Window Glass	4.80	Proprietry	4.30	No Lead	100000
	Ni Plating	3.00	Ni	3.00	100.00	100000
Total		97.40				



Pb-free Lens Cap Reliability Qualification Report, (Supplier – Wuhan Risen Tech)

1 Revision History

Version	ECO	Date	Modifications / Changes
0	ECO-034727	Dec 2016	New document

2 Contents

1	Revision History	2
2	Contents	
3	Purpose	3
4	Reliability Qualification Stresses	3
4.1	Qualification Tests	3
4.2	Temperature Cycling Test Drift Analysis (500 cycles)	4
4.3	MS/MV Drift Analysis (1500G, 20-2000Hz)	6
4.4	Residual Gas Analysis Results	7
5	Conclusion	8

3 Purpose

The purpose of this report is to document the qualification of Pb-free lens cap for the ROSA products. The lens cap is supplied by Wuhan Risen Tech Co., Ltd.

4 Reliability Qualification Stresses

4.1 Qualification Tests

Table 1.: Qualification Stresses

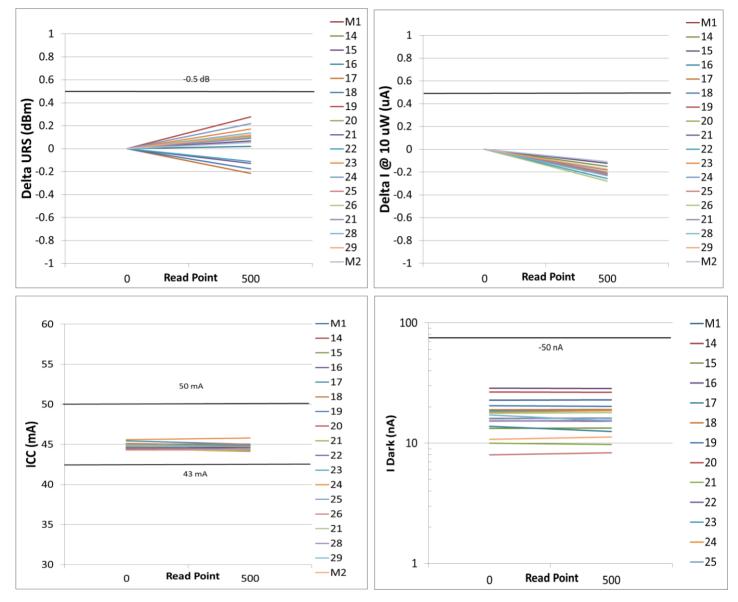
Test	Sample size	Condition	Results
Hermelicity	100pcs	Normal fine leak test, Normal gross leak test	Passed
Temperature Cycling	13pcs	GR-468 Method 3.3.2.2, -40C- 85C,10C/min ramp, 15 min dwell time, 500 cycles	Passed
Mechanical Shock	13pcs	GR-468 Method 3.3.1.1 1500g, 1 ms, 5 times/direction, 6directions	Passed
Mechanical Vibration	Same parts with MS	GR-468 Method 3.3.1.1 20 g, 20 to 2000 to 20 Hz, 4 min/cy, 4 cy/axis	Passed
RGA	5	NA	Passed

4.2 Pass Fail Criteria

Table 2.: Qualification Stresses	
Parameter	Criterion
Unstressed receiver sensitivity (URS)	Change > 1 dB
Dark Current	> 50 nA
ICC	Delta of 10%
RSSI at 10 uW	Change > 1 dB

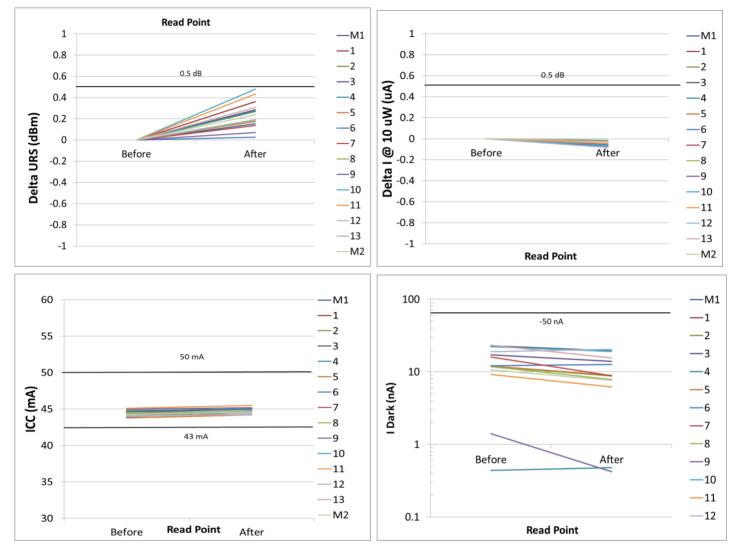
Temperature Cycling Test Drift Analysis (500 cycles)

M1 and M2 are control parts.



4.3 MS/MV Drift Analysis (1500G, 20-2000Hz)

M1 and M2 are control parts.



4.4 Residual Gas Analysis Results

SAMPLE	D	1	2	3	4	5
INLET PRESSURE	torr	4.2	3.9	3.9	3.8	4.0
NITROGEN	%∨	98.3	98.0	97.6	97.7	97.5
OXYGEN	ppm∨	ND	ND	ND	ND	ND
ARGON	%∨	1.38	1.34	1.38	1.37	1.36
CO2	ppmv	385	362	488	400	363
MOISTURE	ppmv	898	909	1,556	1,693	713
HYDROGEN	ppmv	1,538	5,612	7,673	7,435	9,962
METHANE	ppm∨	ND	ND	ND	ND	ND
AMMONIA	ppm∨	ND	ND	ND	ND	ND
HELIUM	ppmv	ND	ND	ND	ND	ND
FLUORO- CARBONS	ppmv	ND	ND	ND	ND	ND

The RGA content of samples built with Risen cap is acceptable.

5 Conclusion

The Risen lead-free cap is compliant and reliable and can be used in the ROSA products.



GN3250 Characterization Report

(Pb-free lens cap from Risen)

Author: Alain Bouchard



Revision List

Revision	Author	Description of change	Revision Date (mm/dd/yyyy)	ECO#
А	Alain Bouchard	First Issue	10/04/2016	033675



Table of Contents

1.	S	cope		6
2.	Ν	/lethod .		6
3.	R	esults		6
	3.1.	. Supp	oly Current (I _{cc})	7
	3	.1.1.	Test Descriptions	7
	3	.1.2.	I _{cc} (no optical input)	8
	3	.1.3.	I _{cc} (0.5dBm avg. optical power @ 1310nm)	9
	3	.1.4.	I _{cc} (0.5dBm avg. optical power @ 1550nm)	10
	3.2.	. Resp	oonsivity, RSSI Dark	11
	3	.2.1.	Test Descriptions	11
	3	.2.2.	Responsivity (A/W) at 1310nm	12
	3	.2.3.	Responsivity (A/W) at 1550nm	13
	3	.2.4.	RSSI dark (nA)	14
	3.3.	. Opti	cal Receiver Sensitivity	15
	3	.3.1.	Test Descriptions	15
	3	.3.2.	Unstressed Receiver Sensitivity at 1310nm and 11.3Gbps (dBm OMA)	17
	3	.3.3.	Unstressed Receiver Sensitivity at 1550nm and 11.3Gbps (dBm OMA)	18
	3	.3.1.	Unstressed Receiver Sensitivity at 1310nm and 10.3125Gbps (dBm OMA)	19
	3	.3.2.	Unstressed Receiver Sensitivity at 1550nm and 10.3125Gbps (dBm OMA)	20
	3	.3.3.	Stressed Receiver Sensitivity at 1310nm and BaseL (dBm OMA)	21
	3	.3.4.	Stressed Receiver Sensitivity at 1550nm and BaseL (dBm OMA)	22
	3	.3.5.	Stressed Receiver Sensitivity at 1310nm and BaseE (dBm OMA)	23
	3	.3.6.	Stressed Receiver Sensitivity at 1550nm and BaseE (dBm OMA)	24
	3.4.	. Opti	cal Overload	25
	3	.4.1.	Test Descriptions	25
	3	.4.2.	Overload at 1310nm and 11.3Gbps (Avg. power dBm)	26
	3	.4.3.	Overload at 1550nm and 11.3Gbps (Avg. power dBm)	27
	3	.4.4.	Overload at 1310nm and 10.3125Gbps (Avg. power dBm)	28



3.4	l.5.	Overload at 1550nm and 10.3125Gbps (Avg. power dBm)	29
3.5.	Elec	ctrical Output Eyes	30
3.5	5.1.	Test Descriptions	30
3.5	5.2.	Typical Eye Diagrams at 25C	31
3.5	5.1.	Typical Eye Diagrams at -40C	32
3.5	5.2.	Typical Eye Diagrams at 85C	33
3.5	5.3.	Typical Eye Diagrams at 95C	34
3.5	5.4.	Crossing Percentage at -18 dBm avg. Power at 1550nm and 11.3Gbps	35
3.5	5.5.	Rise Time at -18 dBm avg. Power at 1550nm and 11.3Gbps	36
3.5	. 6.	Fall Time at -18 dBm avg. Power at 1550nm and 11.3Gbps	37
3.5	5.7.	Height at -18 dBm avg. Power at 1550nm and 11.3Gbps	38
3.5	5.8.	Amplitude at -18 dBm avg. Power at 1550nm and 11.3Gbps	39
3.5	5.9.	Jitter pk-pk at -18 dBm avg. Power at 1550nm and 11.3Gbps	40
3.5	5.10.	Jitter RMS at -18 dBm avg. Power at 1550nm and 11.3Gbps	41
3.5	5.11.	Crossing Percentage at -10 dBm avg. Power at 1550nm and 11.3Gbps	42
3.5	5.12.	Rise Time at -10 dBm avg. Power at 1550nm and 11.3Gbps	43
3.5	5.13.	Fall Time at -10 dBm avg. Power at 1550nm and 11.3Gbps	44
3.5	5.14.	Height at -10 dBm avg. Power at 1550nm and 11.3Gbps	45
3.5	5.15.	Amplitude at -10 dBm avg. Power at 1550nm and 11.3Gbps	46
3.5	5.16.	Jitter pk-pk at -10 dBm avg. Power at 1550nm and 11.3Gbps	47
3.5	5.17.	Jitter RMS at -10 dBm avg. Power at 1550nm and 11.3Gbps	48
3.5	5.18.	Crossing Percentage at +1.6 dBm avg. Power at 1550nm and 11.3Gbps	49
3.5	5.19.	Rise Time at +1.6 dBm avg. Power at 1550nm and 11.3Gbps	50
3.5	5.20.	Fall Time at +1.6 dBm avg. Power at 1550nm and 11.3Gbps	51
3.5	5.21.	Height at +1.6 dBm avg. Power at 1550nm and 11.3Gbps	52
3.5	5.22.	Amplitude at +1.6 dBm avg. Power at 1550nm and 11.3Gbps	53
3.5	5.23.	Jitter pk-pk at +1.6 dBm avg. Power at 1550nm and 11.3Gbps	54
3.5	5.24.	Jitter RMS at +1.6 dBm avg. Power at 1550nm and 11.3Gbps	55
3.6.	S-pa	arameters	56
3.6	5.1.	Test Descriptions	56
3.6	ö.2.	P-Channel S21 plots at 1550nm and -19dBm Optical Input Power	57



	2	C D	GENNUM PRODUCTS	- 0						
	3.	6.3.	P-Channel S22 plots at 1550nm and 0dBm electrical input power	58						
	3.	6.4.	N-Channel S22 plots at 1550nm and 0dBm electrical input power	59						
	3.	3.6.5. S21 -3dB Bandwidth (GHz) at 1550nm								
	3.	6.6.	Group Delay (ps) at 1550 nm (6GHz)	61						
4.	N	otes an	d Conclusions	62						
5.	A	ppendix	1: Eye Diagram Measurement Definitions	1						
а	ı.	Eye He	ights	1						
b).	Eye An	nplitudes	3						
C		Jitter R	MS and pk-pk	4						
c	۱.	Crossir	ng percentage	5						
e	2.	Rise Ti	me and Fall Time	6						



1. Scope

This document contains a summary of the results of the characterization testing performed on GN3250 ROSA using Pb-free glass seal lens cap from Risen.

2. Method

The GN3250 with LC optical receptacles (barrels) were tested using a Semtech designed evaluation board. These evaluation boards feature controlled impedance lines that are terminated in SMA connectors, and permit full assessment of the electrical properties of the ROSA using input from optical excitation at a wide range of frequencies.

Characterization plan is Gendoc 53406.

3. Results



3.1. Supply Current (I_{CC})

3.1.1. Test Descriptions

In these tests the ROSA was powered up and the current into the V_{cc} pin was measured. During the test the RSSI pin was pulled to ground. The test was performed under the following conditions:

- 1) No optical power input into the ROSA, i.e. $P_0=0$ mW. This is to test the dark condition.
- 2) 0.5dBm of avg. optical power

The optical signal input to the ROSA was unmodulated. Test was done at both 1310nm and 1550nm.

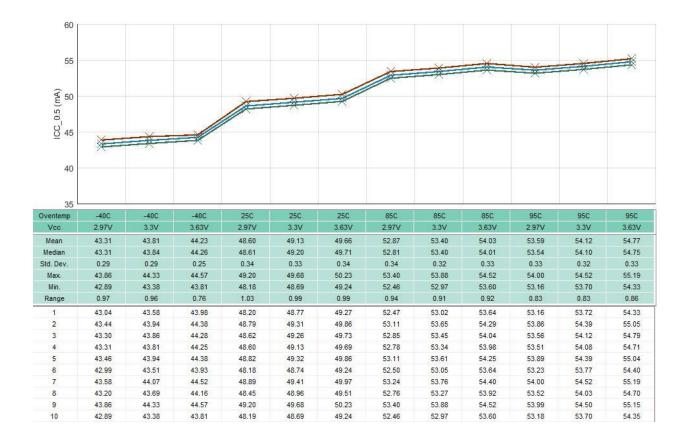


3.1.2. I_{CC} (no optical input)





3.1.3. I_{CC} (0.5dBm avg. optical power @ 1310nm)





3.1.4. I_{CC} (0.5dBm avg. optical power @ 1550nm)





3.2. Responsivity, RSSI Dark

3.2.1. Test Descriptions

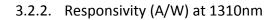
Responsivity is calculated by dividing the measured the RSSI current by the input optical power at an input optical power of -10dBm (100uW). The input optical signal is unmodulated.

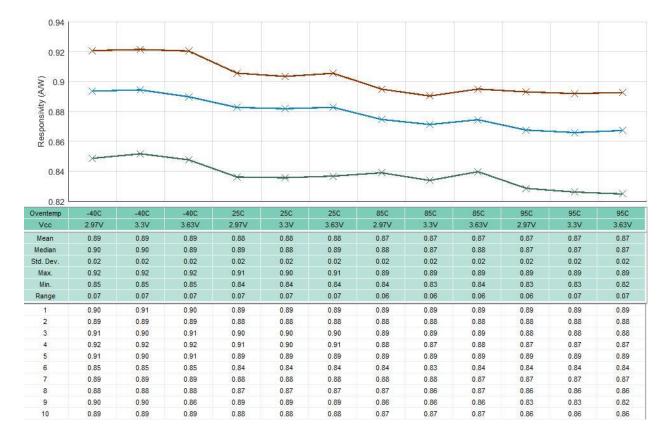
In these tests the ROSA was powered up and the current sunk from the RSSI pin was measured. During the test the RSSI pin was pulled to ground. The test was performed under the following conditions:

- 1) No optical power input into the ROSA, i.e. $P_0=0$ mW. This is to test the dark condition.
- 2) -10dBm of avg. optical power

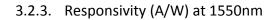
The optical signal input to the ROSA was unmodulated. Test was done at both 1310nm and 1550nm.

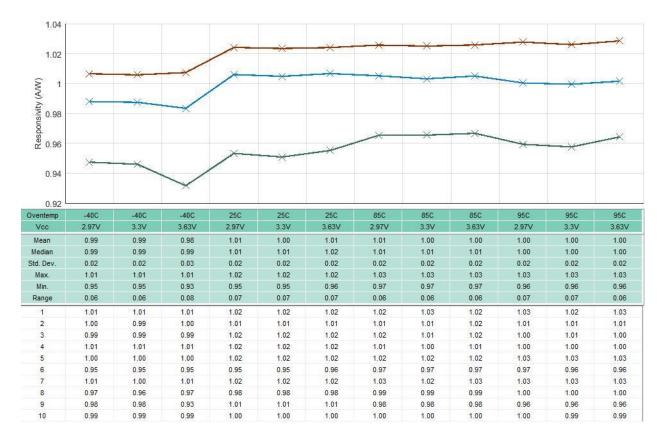














3.2.4. RSSI dark (nA)





3.3. Optical Receiver Sensitivity

3.3.1. Test Descriptions

The receiver sensitivity tests were performed by performing a sweep of optical powers and recording the BER for those optical powers.

In the case of 10.3125 and 11.3 data rates the output of the ROSA is passed through a GN2013 CDR before reaching the BERT. This is done because the sensitivity of the GN2013 CDR is much better than the BERT inputs and allows for a much better measurement of the true sensitivity of the ROSA.

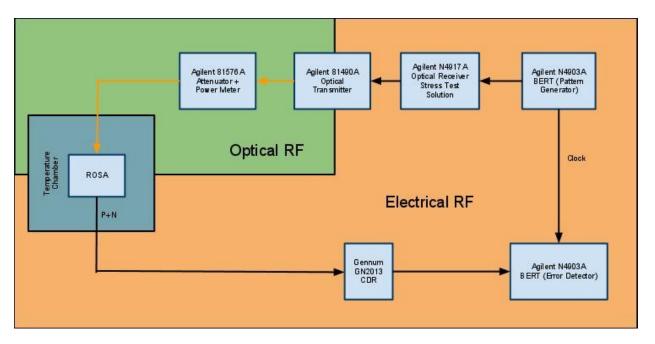


Figure 1. Sensitivity testing Block Diagram.



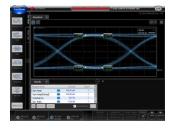


Figure 2. 1310nm 11.3Gbps Input Eye

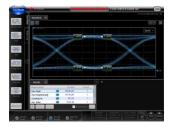


Figure 4. 1310nm 10.3125Gbps Input Eye

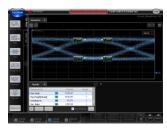


Figure 6. 1310 BaseL Input Eye

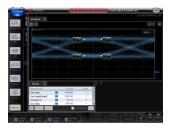


Figure 8. 1310 BaseE Input Eye

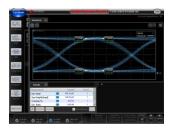


Figure 3. 1550nm 11.3Gbps Input Eye

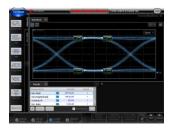


Figure 5. 1550nm 10.3125Gbps Input Eye

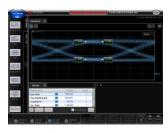


Figure 7. 1550 BaseL Input Eye

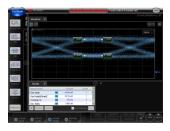


Figure 9. 1550 BaseE Input Eye



3.3.2. Unstressed Receiver Sensitivity at 1310nm and 11.3Gbps (dBm OMA)





3.3.3. Unstressed Receiver Sensitivity at 1550nm and 11.3Gbps (dBm OMA)





3.3.1. Unstressed Receiver Sensitivity at 1310nm and 10.3125Gbps (dBm OMA)





3.3.2. Unstressed Receiver Sensitivity at 1550nm and 10.3125Gbps (dBm OMA)





3.3.3. Stressed Receiver Sensitivity at 1310nm and BaseL (dBm OMA)





3.3.4. Stressed Receiver Sensitivity at 1550nm and BaseL (dBm OMA)

-15												
(IIIIg0) (YMO) 71-41 - 710 - 15.516161617 -									~		×-	- ×
-16			×		<u>×</u>			*	×	×	×	×
-16.5	× -			*	×	*			Tell. Marchine and	\checkmark		
-17	×	X		~								
-17.5	×											
entemp	-40C	-40C	-40C	25C	25C	25C	85C	85C	85C	95C	95C	95C
Vcc	2.97V	3.3V	3.63V	2.97V	3.3V	3.63V	2.97V	3.3V	3.63V	2.97V	3.3V	3.63\
lean	-16.82	-16.65	-16.61	-16.53	-16.35	-16.38	-16.12	-15.95	-15.86	-16.02	-15.78	-15.7
edian	-16.81	-16.58	-16.60	-16.44	-16.32	-16.36	-16.07	-15.92	-15.80	-15.96	-15.73	-15.6
l. Dev.	0.27	0.26	0.27	0.19	0.17	0.16	0.16	0.15	0.17	0.19	0.18	0.20
lax.	-16.38	-16.36	-16.21	-16.32	-16.10	-16.13	-15.93	-15.73	-15.68	-15.75	-15.47	-15.4
Min.	-17.21	-17.06	-17.04	-16.82	-16.54	-16.65	-16.38	-16.22	-16.15	-16.40	-16.03	-16.0
ange	0.83	0.70	0.83	0.50	0.43	0.52	0.45	0.49	0.47	0.66	0.56	0.61
1	-16.77	-16.61	-16.49	-16.36	-16.27	-16.35	-16.13	-15.95	-15.84	-15.97	-15.66	-15.5
2	-16.99	-16.67	-16.89	-16.32	-16.23	-16.39	-15.99	-15.87	-15.68	-15.94	-15.75	-15.6
3	-16.67	-16.54	-16.36	-16.38	-16.10	-16.30	-16.04	- <mark>16.0</mark> 1	-15.92	-16.04	-15.69	-15.7
4	-17.08	-16.94	-16.68	-16.82	-16.51	-16.51	-16.06	-15.88	-15.74	-15.95	-15.68	-15.6
5	-16.86	-16.54	-16.73	-16.81	-16.53	-16.36	-16.27	-16.10	-16.06	-16.17	-16.03	-15.9
6	-16.63	-16.36	-16.37	-16.41	-16.17	-16.13	-15.93	-15.83	-15.73	-15.89	-15.71	-15.5
7	-17.21	-16.99	-16.84	-16.68	-16.54	-16.59	-16.32	-16.08	-16.05	-16.18	-15.96	-15.9
8	-16.58	-16.46	-16.51	-16.48	-16.25	-16.21	-16.07	-15.83	-15.76	-15.93	-15.80	-15.7
9	-16.38	-16.36	-16.21	-16.38	-16.37	-16.35	-15.97	-15.73	-15.69	-15.75	-15.47	-15.4
10	-17.09	-17.06	-17.04	-16.63	-16.54	-16.65	-16.38	-16.22	-16.15	-16.40	-16.00	-16.00



3.3.5. Stressed Receiver Sensitivity at 1310nm and BaseE (dBm OMA)

-14												
(Iugo) (Yulo) 7151515151616								- 		*	×	
-15					```````			*		\geq	*	X
-15.5	×	×		*		*	*			6.7		
-16	×		>		2.3							
-16.5	-40C	-40C	-40C	25C	25C	25C	85C	85C	85C	95C	95C	95C
Vcc	2.97V	3.3V	3.63V	2.97V	3.3V	3.63V	2.97V	3.3V	3.63V	2.97V	3.3V	3.63\
lean	-15.94	-15.83	-15.75	-15.54	-15.39	-15.34	-15.10	-14.85	-14.78	-14.95	-14.69	-14.6
edian	-15.94	-15.80	-15.79	-15.53	-15.38	-15.32	-15.11	-14.79	-14.78	-14.95	-14.75	-14.5
. Dev.	0.22	0.24	0.20	0.16	0.18	0.16	0.13	0.18	0.16	0.16	0.19	0.17
lax.	-15.57	-15.49	-15.49	-15.30	-15.15	-15.10	-14.91	-14.64	-14.54	-14.66	-14.37	-14.3
Ain.	-16.23	-16.26	-16.04	-15.76	-15.72	-15.63	-15.31	-15.20	-15.10	-15.15	-14.94	-14.8
ange	0.67	0.77	0.56	0.46	0.57	0.53	0.40	0.56	0.56	0.49	0.57	0.57
1	-15.85	-15.80	-15.54	-15.31	-15.19	-15.27	-15.03	-14.83	-14.78	-14.82	-14.37	-14.4
2	-16.13	-15.85	-15.84	-15.45	-15.35	-15.40	-14.97	-14.71	-14.67	-14.95	-14.60	-14.4
3	-15.85	-15.79	-15.53	-15.30	-15.15	-15.16	-15.20	-14.77	-14.61	-14.84	-14.60	-14.5
4	-16.23	-16.09	-15.98	-15.76	-15.72	-15.49	-15.18	-14.71	-14.80	-14.87	-14.80	-14.5
5	-16.07	-15.53	-15.88	-15.60	-15.43	-15.36	-15.18	-15.12	-14.92	-15.12	-14.85	-14.7
6	-15.57	-15.70	-15.56	-15.54	-15.24	-15.10	-14.96	-14.76	-14.69	-14.94	-14.76	-14.5
7	-16.03	-16.02	-15.85	-15.69	-15.61	-15.47	-15.21	-14.94	-14.89	-15.13	-14.83	-14.8
8	-15.71	-15.80	-15.75	-15.48	-15.41	-15.27	-15.05	-14.81	-14.78	-14.99	-14.73	-14.6
9	-15.82	-15.49	-15.49	-15.53	-15.27	-15.26	-14.91	-14.64	-14.54	-14.66	-14.39	-14.3
10	-16.17	-16.26	-16.04	-15.74	-15.50	-15.63	-15.31	-15.20	-15.10	-15.15	-14.94	-14.8



3.3.6. Stressed Receiver Sensitivity at 1550nm and BaseE (dBm OMA)

-14.5												
(iugo) (Yulo) 71516 -								*				×
-15.5					-*					~	×	X
!	×											
-16		×	```		×							
i i	×				-151							
-16.5												
	X											
-17 - entemp	-40C	-40C	-40C	25C	25C	25C	85C	85C	85C	95C	95C	95C
Vcc	2.97V	3.3V	3.63V	2.97V	3.3V	3.63V	2.97V	3.3V	3.63V	2.97V	3.3V	3.63V
lean	-16.33	-16.14	-16.08	-15.94	-15.80	-15.83	-15.63	-15.43	-15.30	-15.47	-15.26	-15.20
edian	-16.32	-16.06	-16.09	-15.89	-15.75	-15.81	-15.58	-15.40	-15.24	-15.43	-15.23	-15.17
I. Dev.	0.33	0.29	0.26	0.21	0.20	0.20	0.18	0.17	0.17	0.19	0.18	0.16
lax.	-15.84	-15.78	-15.65	-15.64	-15.52	-15.59	-15.43	-15.19	-15.12	-15.21	-15.05	-14.96
Min.	-16.75	-16.59	-16.49	-16.33	-16.13	-16.13	-15.95	-15.75	-15.65	-15.79	-15.55	-15.48
ange	0.91	0.80	0.84	0.68	0.61	0.55	0.52	0.56	0.53	0.57	0.50	0.50
1	-16.31	-16.10	-15.86	-15.68	-15.64	-15.77	-15.60	-15.47	-15.18	-15.29	-15.10	-15.15
2	-16.52	-16.18	-16.34	-15.84	-15.71	-15.85	-15.51	-15.26	-15.14	-15.44	-15.14	-15.05
3	-16.10	-16.01	-15.83	-15.64	-15.52	-15.65	-15.62	-15.44	-15.37	-15.45	-15.24	-15.12
4	-16.68	-16.40	-16.17	-16.11	-16.05	-15.97	-15.52	-15.34	-15.22	-15.36	-15.09	-15.24
5	-16.33	-15.89	-16.13	-16.03	-15.92	-15.91	-15.76	-15.54	-15.42	-15.73	-15.37	-15.33
6	-15.99	-15.78	-15.93	-15.84	-15.63	-15.59	-15.46	-15.34	-15.26	-15.42	-15.23	-15.08
7	-16.75	-16.59	-16.33	-16.33	-16.13	-16.13	-15.88	-15.61	-15.49	-15.68	-15.54	-15.40
8	-15.84	-16.00	-16.05	-15.91	-15.68	-15.65	-15.56	-15.36	-15.18	-15.38	-15.26	-15.20
9	-16.06	-15.85	-15.65	-15.87	-15.79	-15.66	-15.43	-15.19	-15.12	-15.21	-15.05	-14.96
10	-16.73	-16.56	-16.49	-16.14	-15.96	-16.12	-15.95	-15.75	-15.65	-15.79	-15.55	-15.46



3.4. Optical Overload

3.4.1. Test Descriptions

The optical overload is measured by decreasing the average optical power to the ROSA in steps from a suitable power level.

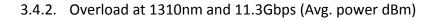
In the case of 10.3125 and 11.3 data rates the output of the ROSA is passed through a GN2013 CDR before reaching the BERT.

In some cases, the overload test was limited by the maximum optical power of the optical transmitter. As a result, the results in the report only represent a lower bound to the performance of the ROSAs. The ROSA performance is better than results presented in some cases. (Worst case is -40C, 11.3G and 1550nm)

The input eyes used are the same as for the sensitivity tests.

The equipment setup is the same as for the sensitivity tests.









3.4.3. Overload at 1550nm and 11.3Gbps (Avg. power dBm)





3.4.4. Overload at 1310nm and 10.3125Gbps (Avg. power dBm)





3.4.5. Overload at 1550nm and 10.3125Gbps (Avg. power dBm)





3.5. Electrical Output Eyes

3.5.1. Test Descriptions

Electrical output eyes of the P channel for the following conditions were measured at 11.3G data rate, unstressed eye at 1550nm wavelength.

Average power of -18dBm
 Average power of -10dBm
 Average power of 1.6dBm

Eye parameter measurements were made single ended. The following was measured.

Crossing Percentage
 Rise Time
 Fall Time
 Eye Height
 Eye Amplitude
 Peak to Peak Jitter
 RMS Jitter

The following tables contain P channel measurements obtained.

The input eyes used are the same as for the sensitivity tests.

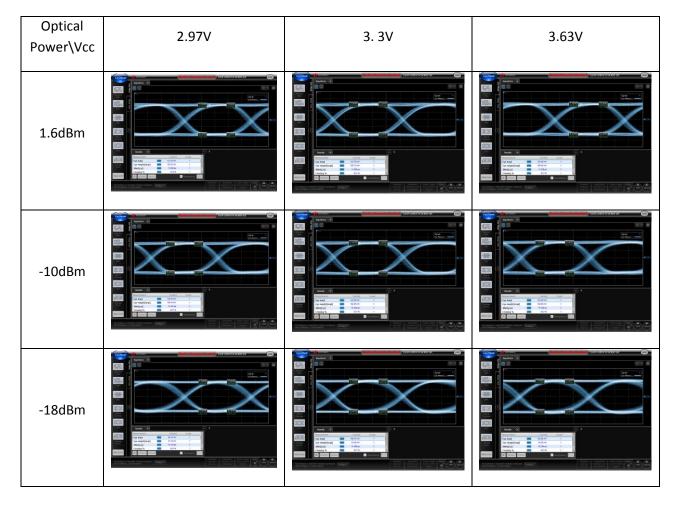
The Jitter measurements are uncorrected for jitter of the source.

Long RF cables had to be used to test the ROSAs in a temperature chamber. Due to the attenuation in the RF cables from the ROSA to the scope, the measured parameters of the output eyes are negatively affected. The measured heights and amplitudes are lower than if the signal was directly measured at the output of the ROSA.

For information on the definitions of the eye diagram measurements see Appendix 1

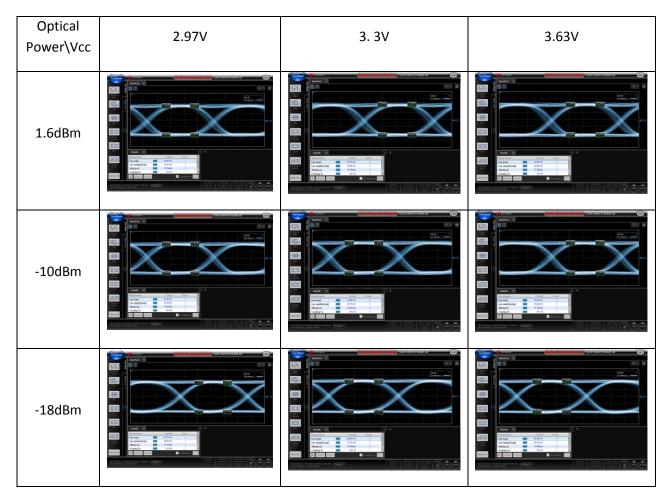


3.5.2. Typical Eye Diagrams at 25C



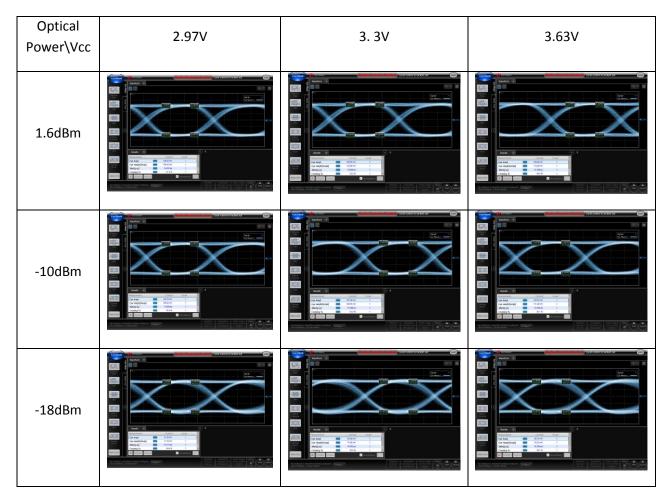


3.5.1. Typical Eye Diagrams at -40C



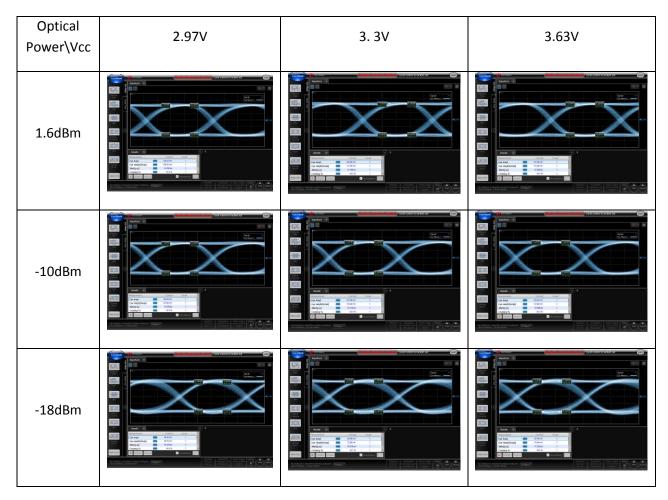


3.5.2. Typical Eye Diagrams at 85C





3.5.3. Typical Eye Diagrams at 95C





3.5.4. Crossing Percentage at -18 dBm avg. Power at 1550nm and 11.3Gbps







3.5.5. Rise Time at -18 dBm avg. Power at 1550nm and 11.3Gbps



3.5.6. Fall Time at -18 dBm avg. Power at 1550nm and 11.3Gbps

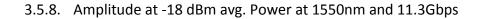






3.5.7. Height at -18 dBm avg. Power at 1550nm and 11.3Gbps











3.5.9. Jitter pk-pk at -18 dBm avg. Power at 1550nm and 11.3Gbps



3.5.10. Jitter RMS at -18 dBm avg. Power at 1550nm and 11.3Gbps





3.5.11. Crossing Percentage at -10 dBm avg. Power at 1550nm and 11.3Gbps





3.5.12. Rise Time at -10 dBm avg. Power at 1550nm and 11.3Gbps





3.5.13. Fall Time at -10 dBm avg. Power at 1550nm and 11.3Gbps





3.5.14. Height at -10 dBm avg. Power at 1550nm and 11.3Gbps





3.5.15. Amplitude at -10 dBm avg. Power at 1550nm and 11.3Gbps





3.5.16. Jitter pk-pk at -10 dBm avg. Power at 1550nm and 11.3Gbps





3.5.17. Jitter RMS at -10 dBm avg. Power at 1550nm and 11.3Gbps





3.5.18. Crossing Percentage at +1.6 dBm avg. Power at 1550nm and 11.3Gbps





3.5.19. Rise Time at +1.6 dBm avg. Power at 1550nm and 11.3Gbps





3.5.20. Fall Time at +1.6 dBm avg. Power at 1550nm and 11.3Gbps





3.5.21. Height at +1.6 dBm avg. Power at 1550nm and 11.3Gbps







3.5.22. Amplitude at +1.6 dBm avg. Power at 1550nm and 11.3Gbps



3.5.23. Jitter pk-pk at +1.6 dBm avg. Power at 1550nm and 11.3Gbps





3.5.24. Jitter RMS at +1.6 dBm avg. Power at 1550nm and 11.3Gbps





3.6. S-parameters

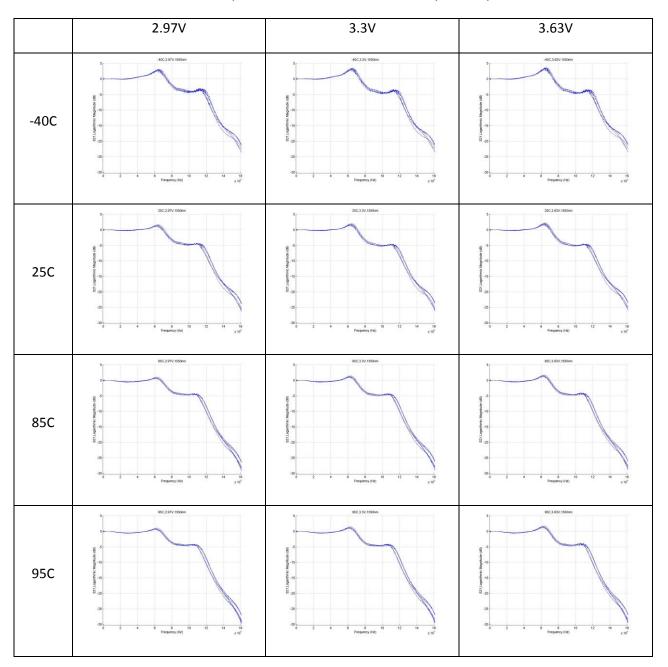
3.6.1. Test Descriptions

An s-parameter sweep was performed with an input optical power of -19dBm and electrical power of 0dBm at 1550nm.

*Note that only 6/10 parts were tested for S-parameters due to equipment availability.



3.6.2. P-Channel S21 plots at 1550nm and -19dBm Optical Input Power



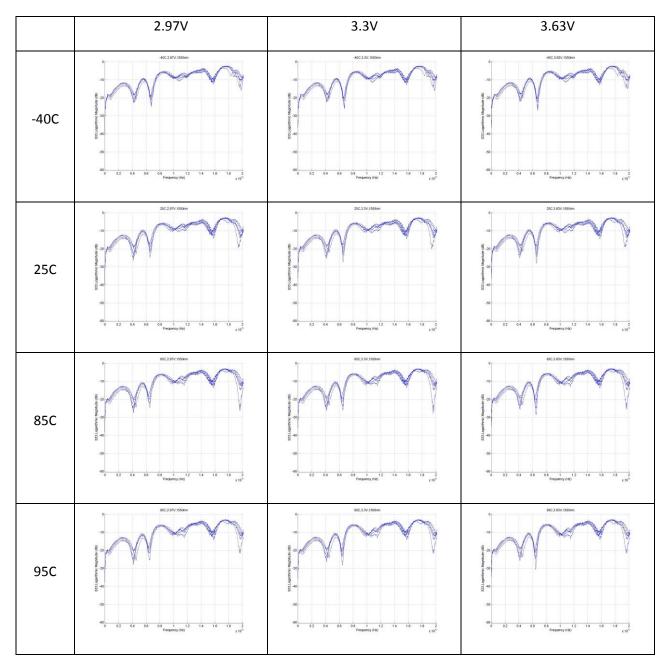


3.6.3. P-Channel S22 plots at 1550nm and 0dBm electrical input power

	2.97V	3.3V	3.63V
-40C	402.287V300m	-00.3.3/199m	403.807/930m
25C	26.2.39V:300m	26.32/1399m	
85C	6C.2 3V.150m	62.32,139m	BCG 3.67V-150m 0 0 0 0 0 0 0 0 0 0 0 0 0
95C	BC.2 JPV:300m	90.324/1990	



3.6.4. N-Channel S22 plots at 1550nm and 0dBm electrical input power



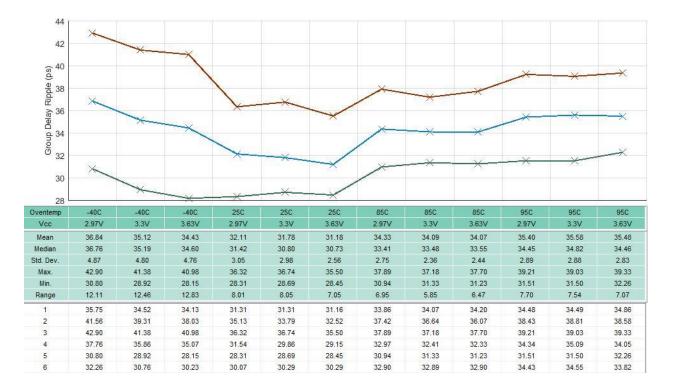


3.6.5. S21 -3dB Bandwidth (GHz) at 1550nm





3.6.6. Group Delay (ps) at 1550 nm (6GHz)





4. Notes and Conclusions

GN3250 ROSA using lead free lens cap shows comparable performance to GN3250 ROSA as documented in PRODDOC4073 characterization report.

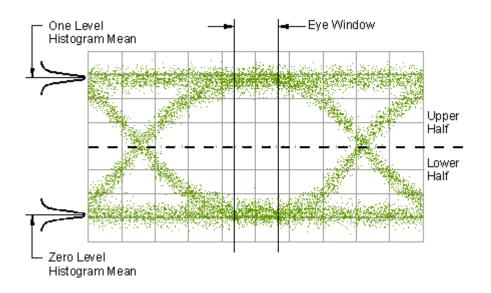
All results satisfy the datasheet.



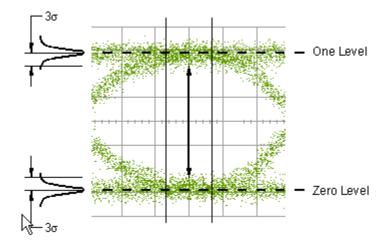
5. Appendix 1: Eye Diagram Measurement Definitions

a. Eye Heights

Eye height is a measure of the vertical opening of an eye diagram. Histograms are constructed to characterize both the one and zero levels *and* their noise levels within the eye window boundaries. The one and zero level measurements are made in a section of the eye referred to as the eye window boundaries. The eye window boundary is the central 20% of the bit period.



The one and zero levels are the relative means of the histograms. The noise is measured through the histograms as three standard deviations from both the one level and zero level into the eye opening.





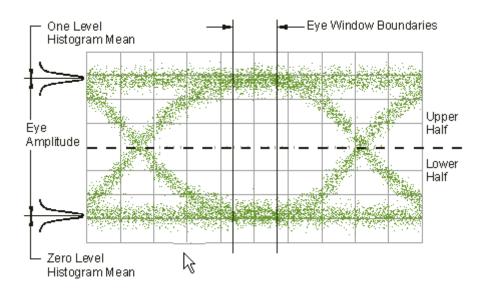
The eye height is determined as follows, eye height = (one level - 3σ) - (zero level + 3σ)



b. Eye Amplitudes

Eye amplitude is the difference between the logic 1 level and the logic 0 level histogram mean values of an eye diagram. This measurement is made in a section of the eye referred to as the eye window boundaries. The eye window boundary is the central 20% of the bit period.

A histogram is constructed using the sampled portion of the eye diagram within the eye window. This histogram is comprised of data points from the upper and lower halves of the eye diagram and is used to determine the mean values of the logic 1 and logic 0 levels. The eye amplitude is determined as follows:

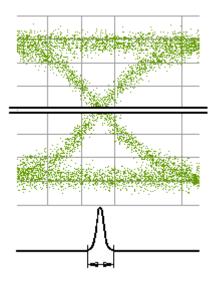




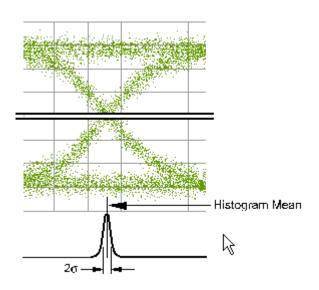
c. Jitter RMS and pk-pk

Eye Jitter is the measure of the time variances of the rising and falling edges of an eye diagram, as these edges affect the crossing point of the eye. To compute jitter, the level of the crossing point of the eye is first determined. Then a vertically thin measurement window is placed horizontally through the crossing point, and a time histogram is generated.

Jitter pk-pk is equal to the full width of the histogram at the eye crossing point.



Jitter RMS is defined as 1 σ (standard deviation) of the crossing point histogram

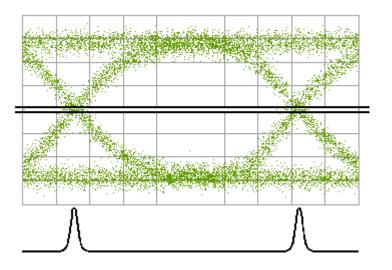




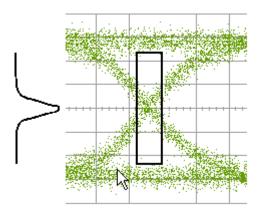
d. Crossing percentage

Crossing percentage is a measure of the amplitude of the crossing points relative to the one level and zero level. The one and zero level measurements are made in a section of the eye referred to as the eye window boundaries. The eye window boundary is the central 20% of the bit period.

A vertically thin measurement window is placed horizontally through the crossing points, and a horizontal histogram is used to determine the mean location (in time) of the crossing point.



A narrow vertical histogram is used to determine the amplitude of crossing points.



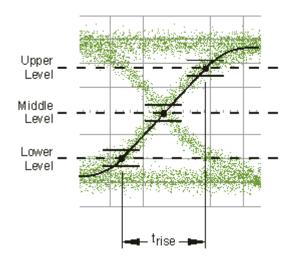
The mean derived from the horizontal and vertical histogram results in V_{cross} . Crossing percentage is then determined by the following:

Crossing percent = 100 (V_{cross}-V_{zero level})/(V_{one level} - V_{zero level})



e. Rise Time and Fall Time

Rise time is a measure of the mean transition time of the data on the upward slope of an eye diagram. The data crosses through the following three thresholds: the lower, middle, and upper thresholds, as well as through the eye crossing point. The settings for the threshold levels are the 20% to 80% points on the transition.



Rise time= time at the upper threshold crossing – time at the lower threshold crossing Fall times are similarly calculated except on the downward slope of an eye diagram.